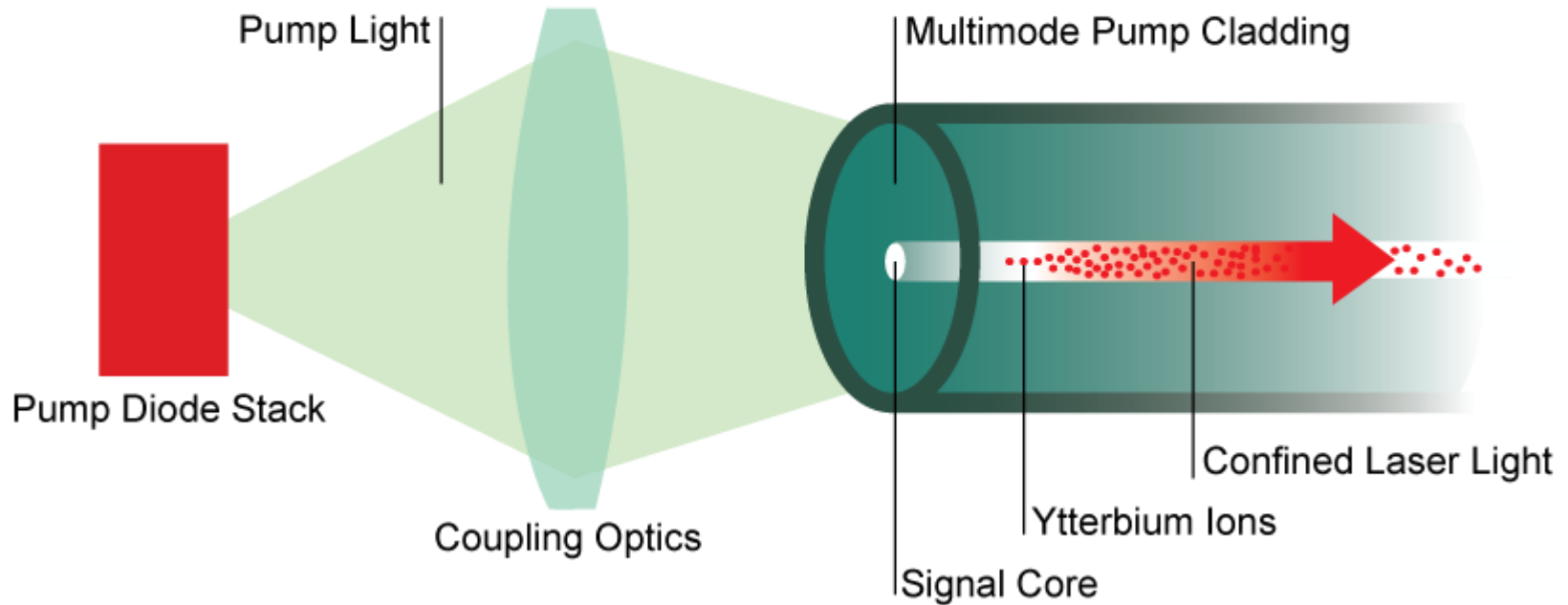




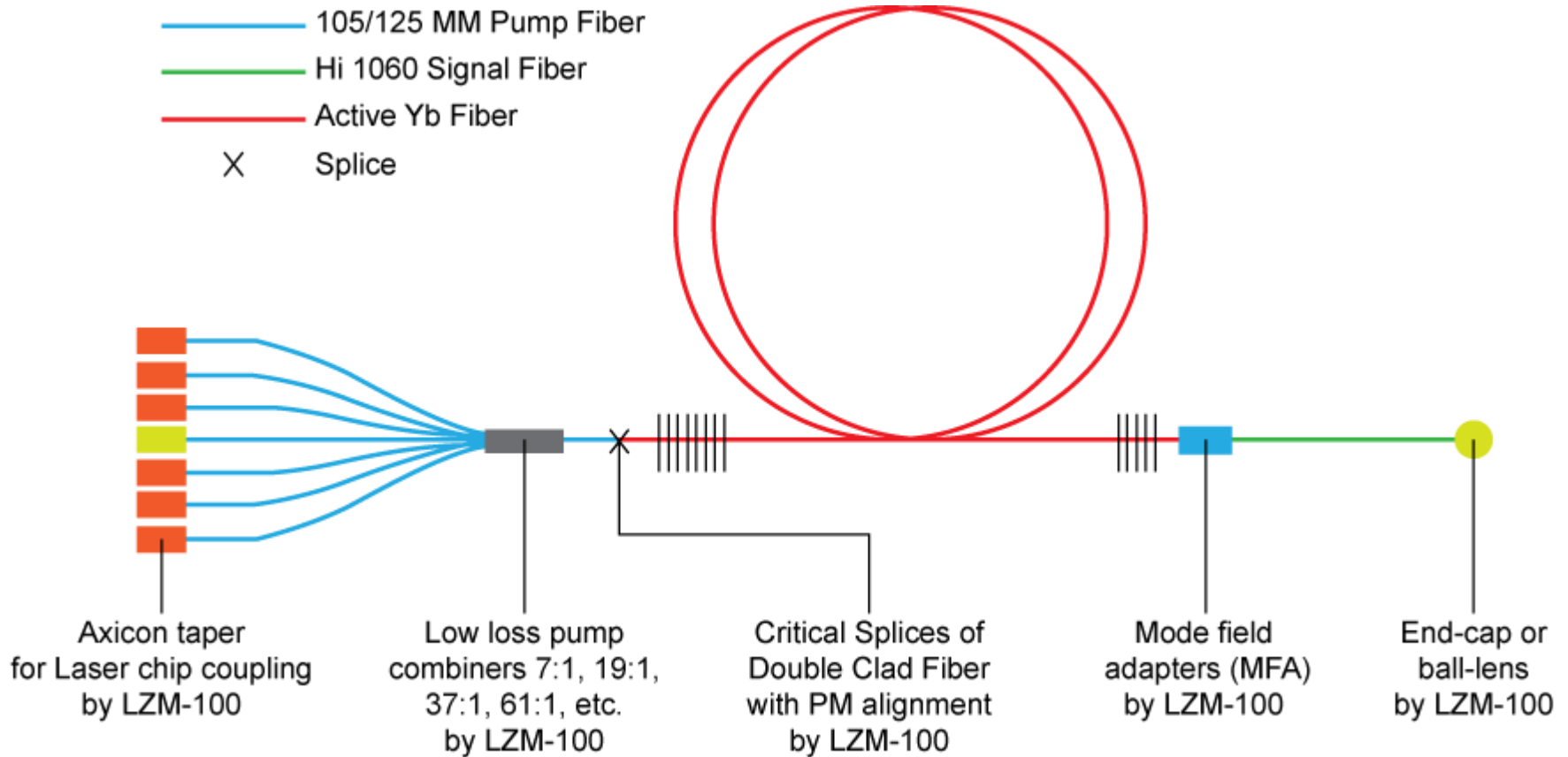
Applications for the LZM-100



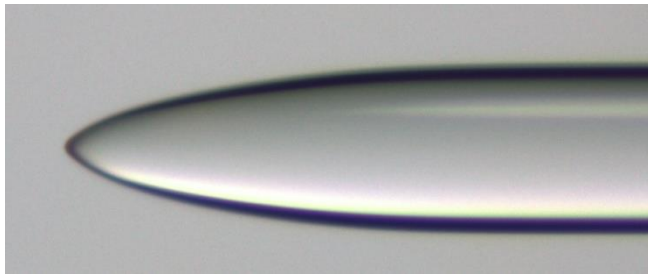


- Multiple pump diodes are used to inject light into the cladding area of a LDF fiber
- The highly doped LDF core absorbs the pump energy as it crosses through the core
- The core emits power at the output wavelength via stimulated emission

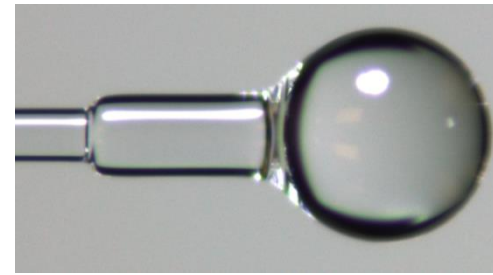
# Typical Fiber Laser Components



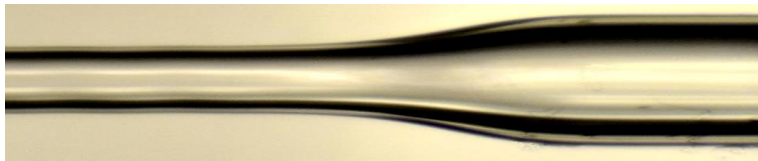
- Typical requirements for the components
  - Lowest possible loss, no contamination, no power leakage
  - Low manufacturing cost
  - Consistent performance



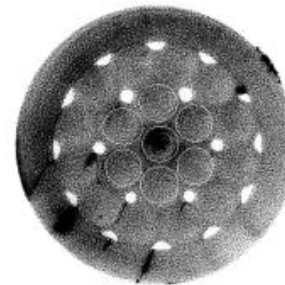
Tapered Axicon with LZM-100



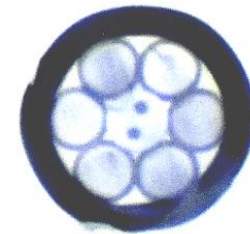
80 μm fiber with 320 μm coreless ball-lens using LZM-100



Tapered capillary made with the LZM-100



Cross section of 19 into 1 combiner with LZM-100



Cross section of 6+1 PM combiner with LZM-100

# Tapered Fused Bundle

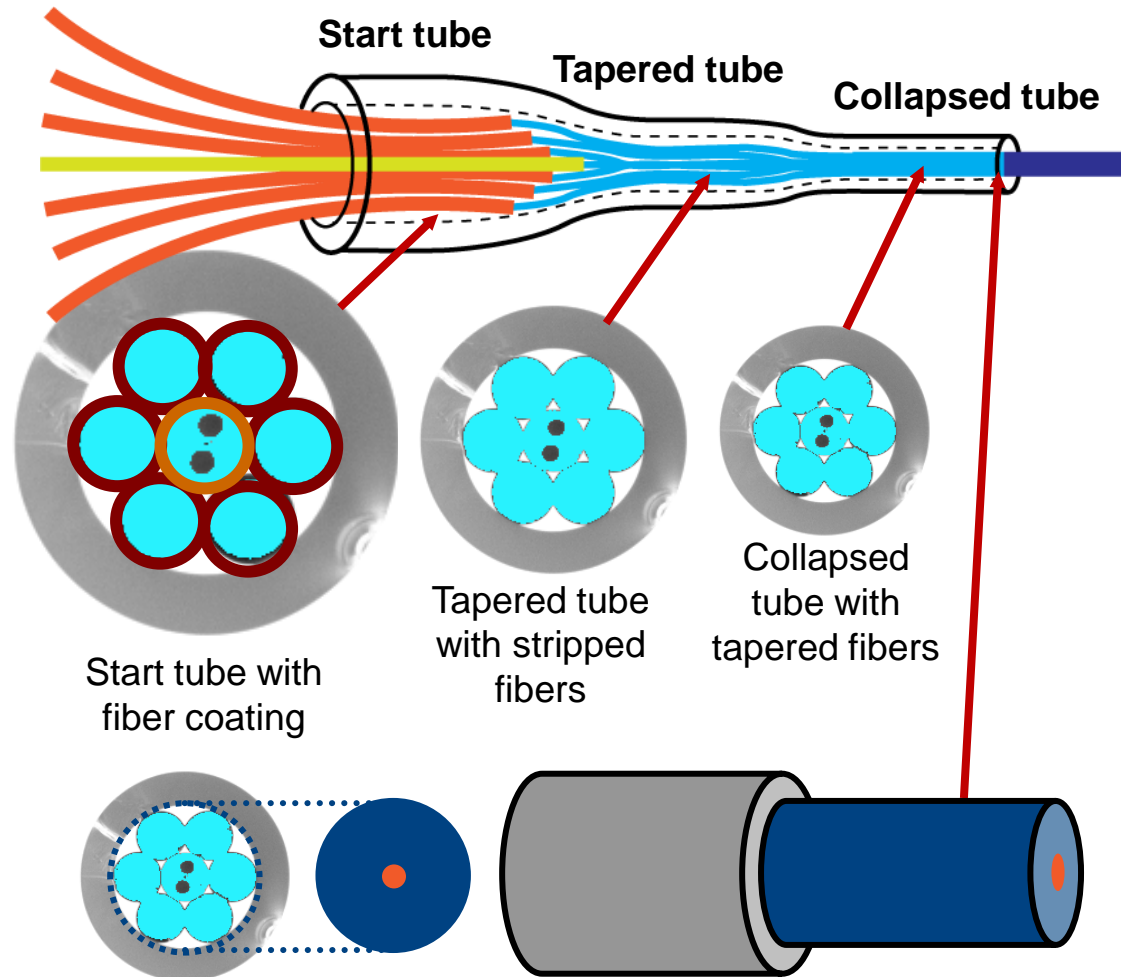
Tube inner diameter  $\sim (2L+1.2) \times OD_{\text{coating}}$

Outer Diameter (OD)  $\sim ID \times 1.4$

L: Layer of fiber; N: Number of fibers

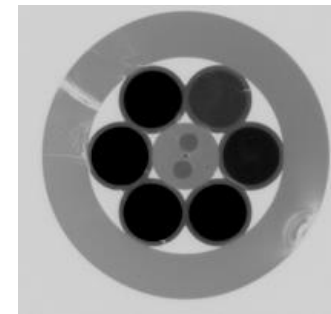
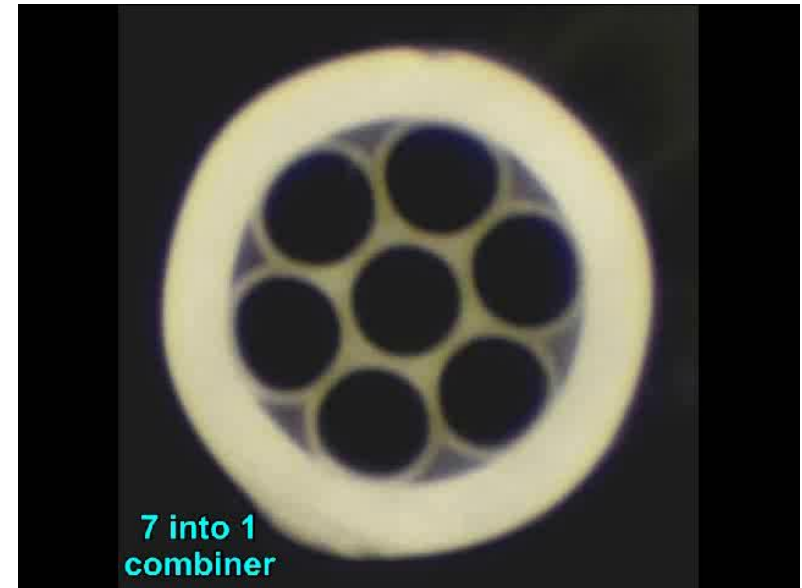
- L=1, N=7, assuming  $OD_{\text{fiber}} = 250 \mu\text{m}$ 
  - ID  $\sim 800 \mu\text{m}$ , OD  $\sim 1120 \mu\text{m}$ ,
  - Taper length 10 – 20 mm
- L=2, N=19,
  - ID  $\sim 1300 \mu\text{m}$ , OD  $\sim 1820 \mu\text{m}$
  - Taper length 16 – 25 mm
- L=3, N=37,
  - ID  $\sim 1800 \mu\text{m}$ , OD  $\sim 2520 \mu\text{m}$
  - Taper length 22 – 30 mm
- L=5, N=91,
  - ID  $\sim 2800 \mu\text{m}$ , OD  $\sim 3920 \mu\text{m}$
  - Taper length 35 – 45 mm
- Where 
$$N = 6 \times \sum_{i=1}^L i + 1$$

A typical tapered fused bundle

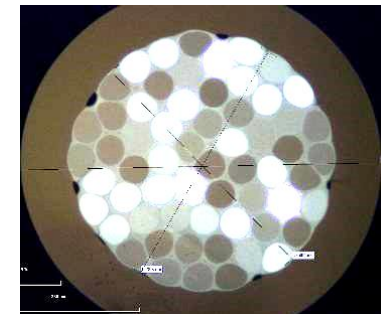


ID of the collapsed tube should match or slightly smaller than the fiber glass OD for DCF to achieve lower splice loss

- Combiner is a key component for fiber laser system, spatial division multiplex for telecomm, etc.
- Many different combiner types have been processed with LZM-100
  - 5 + 1 into 1
  - 6 + 1 into 1
  - 7 into 1
  - 19 into 1
  - 37 into 1
  - 61 into 1
- Basic rules for the combiner design
  - Geometric rule: bundle OD  $\leq$  Output fiber OD for carrying pump power
  - Brightness conservation:  $NA_{in} \times TR \leq NA_{out}$



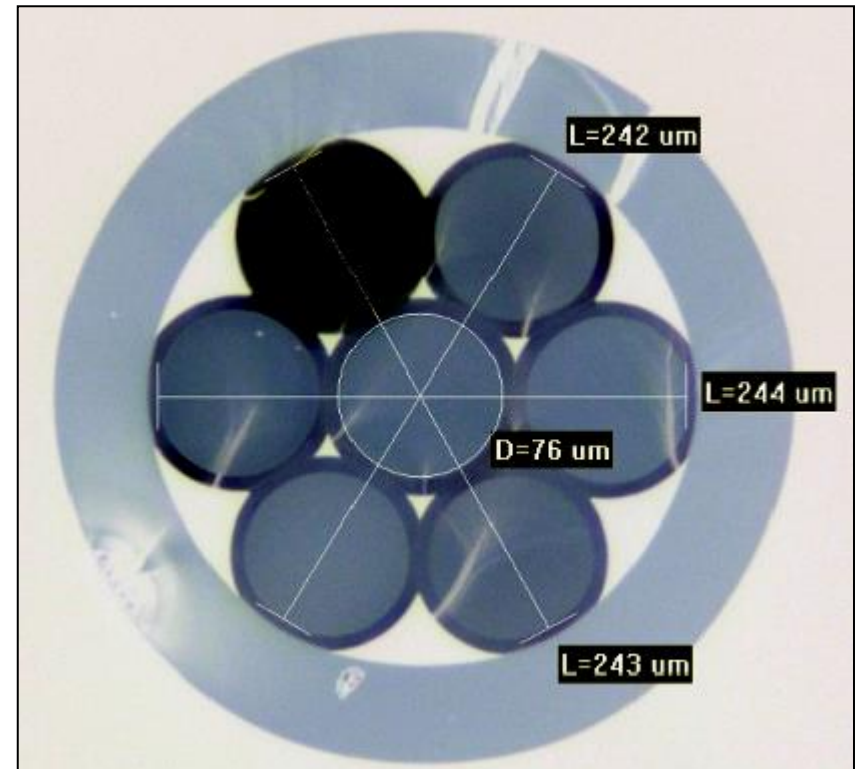
6+1 into 1 combiner



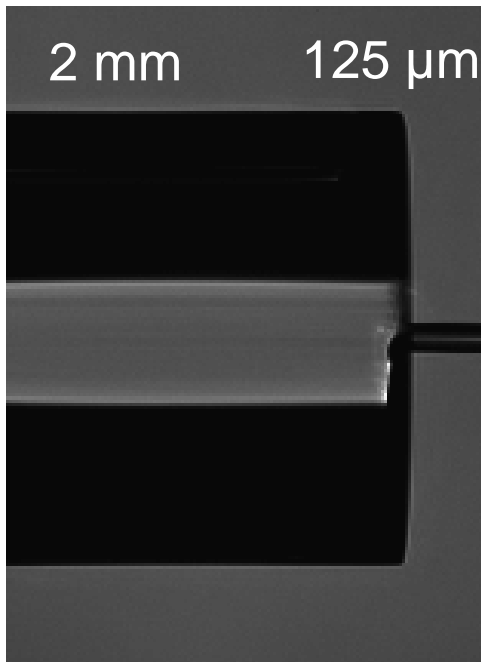
61 into 1 combiner

- 7 into 1 combiner made with LZM-100
- Combiner taper ratio  $TR = 1.67$
- Meet the rule of  $TR \times NA_{input} < NA_{output}$   
( $1.67 \times 0.22 = 0.37 < 0.46$ )
- Max loss = 0.2% (0.01 dB) within measurement noise after packaging

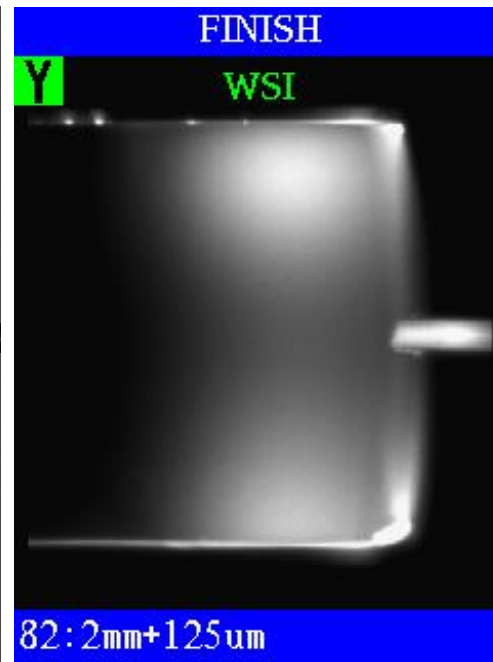
<b>Combiner:</b>	R10 TC7	
<b>Input:</b>	105/125 0.22 NA	
<b>Output:</b>	25/250 0.46 NA	



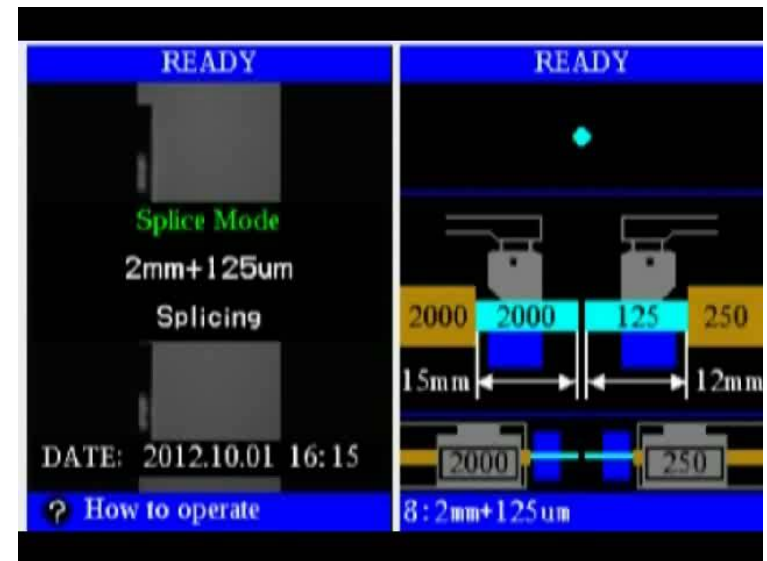
- End-cap splicing with LZM-100 with offsite measurement
- Very high beam quality was achieved with measured M2 value 1.08 to 1.1.
- The splice loss was too low to be measured due to equipment noise
- No temperature change at splices during high power test in kW range



Cold splice image



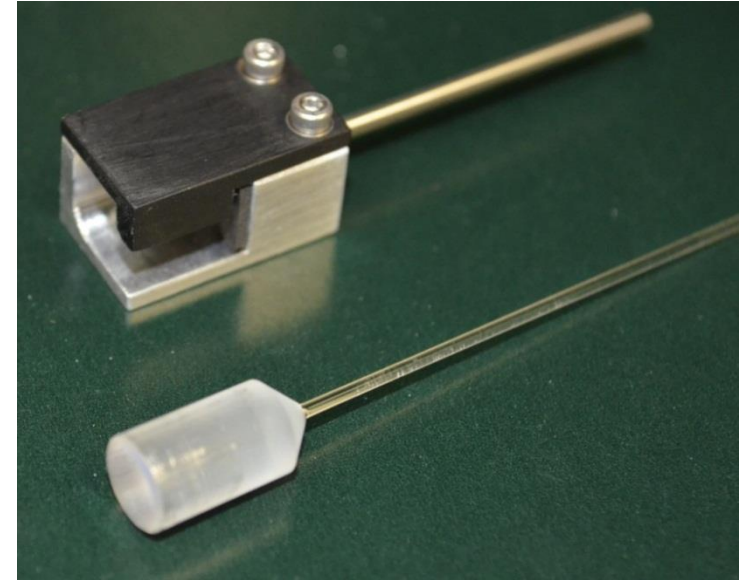
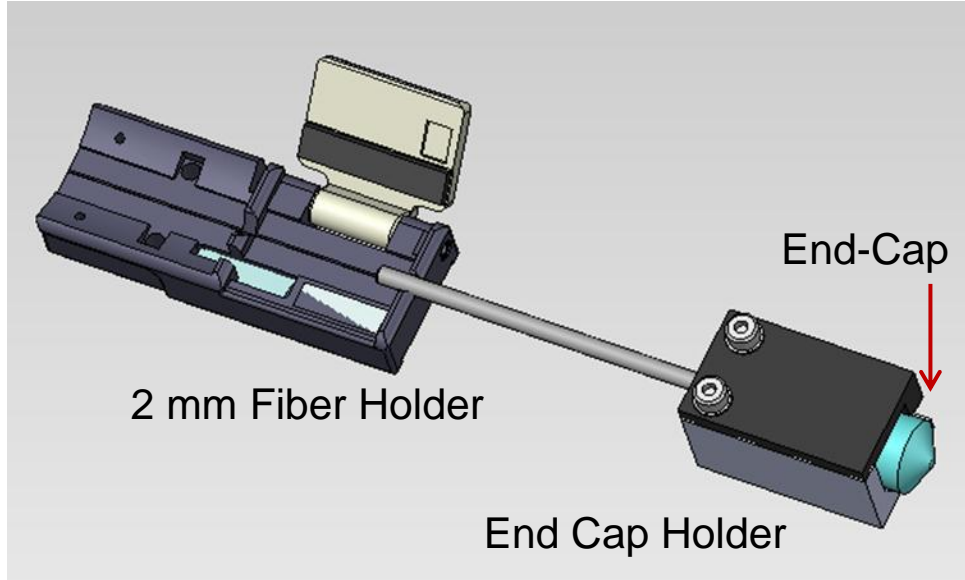
Warm splice image



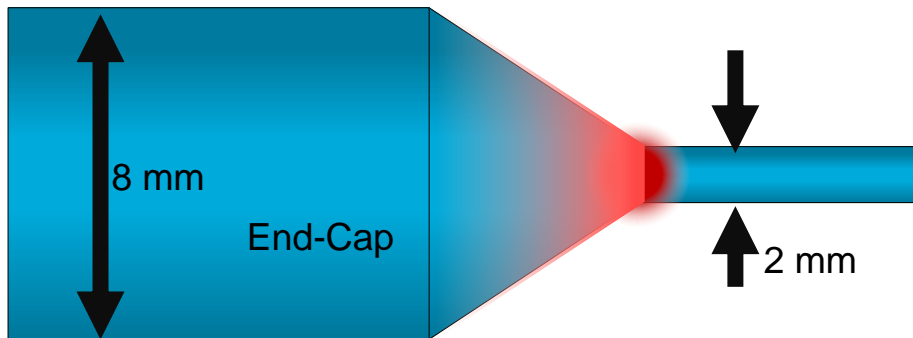
Video

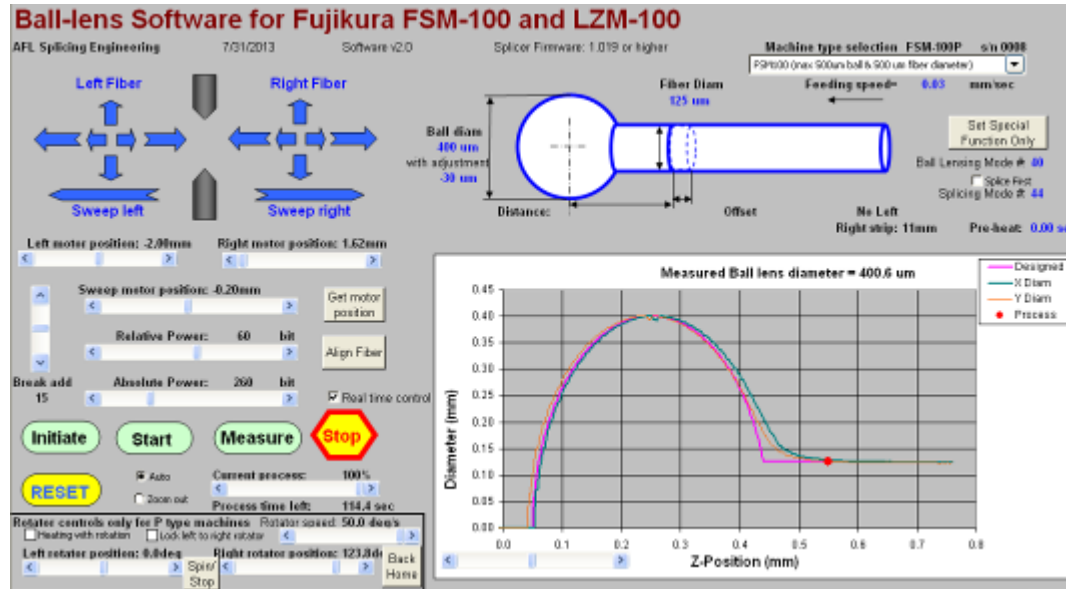


# End-cap Splicing with LZM-100



Sample of end-cap holder and spliced end-cap of 8 mm



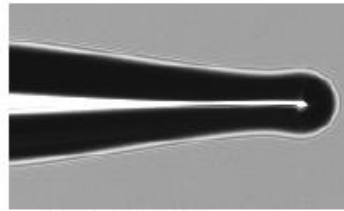


- User friendly software for making ball lens
- Ball size tested up to 2.5 mm diameter
- Largest ball to fiber ratio 1:4.3 (350  $\mu\text{m}$  ball on 80  $\mu\text{m}$  fiber)
- Splicing to coreless fiber and ball-lensing in one run

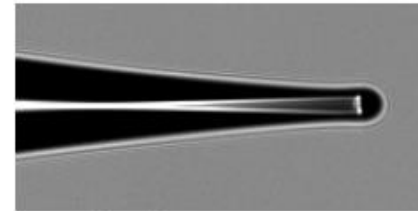
# Different Lens Made with LZM-100



Convex lens



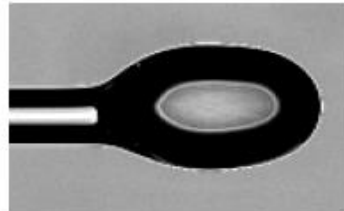
Small ball



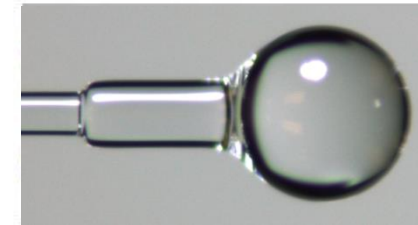
Probe



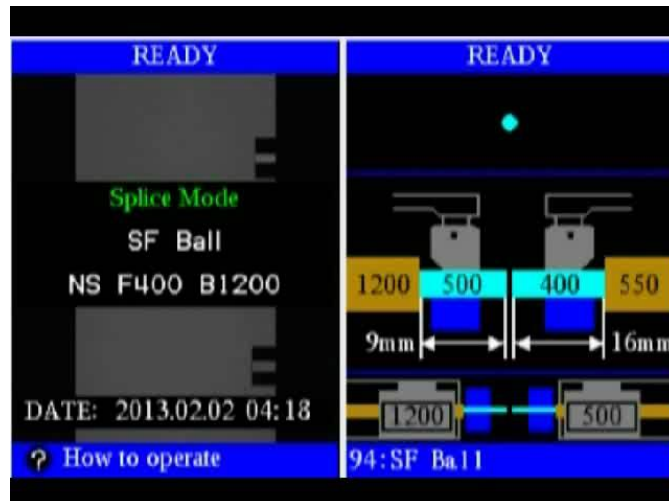
Large ball



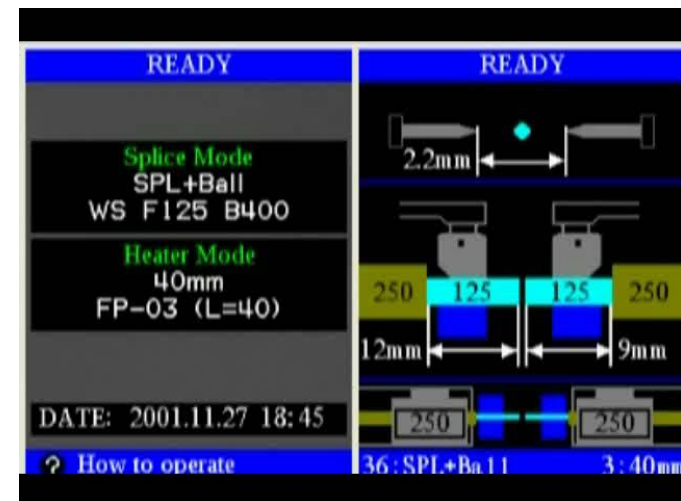
Elongated ball



Spliced ball lens



1200 µm Ball



Video Ball with Splice

$$\Gamma = C \frac{(d - \Lambda_{in})^2 + (\theta \Lambda_{in})^2}{\omega^2} (dB)$$

$\Gamma$ : estimated splice loss

$C$ : constant ( $C = 10 \log_{10} e = 4.34$ )

$\omega$ : mode field radius

$d$ : cladding offset between MCF and SMF

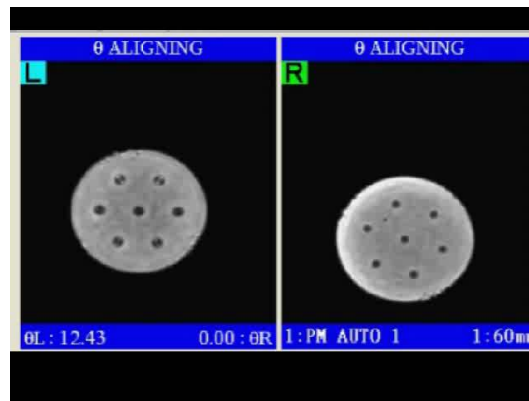
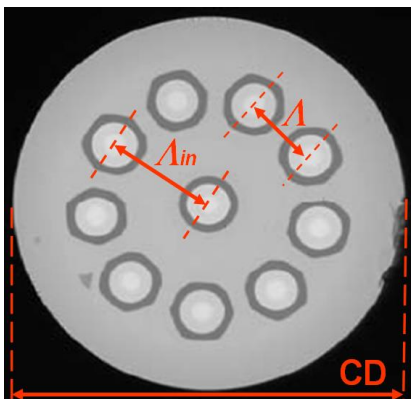
$\theta$ : rotation alignment error

CD: cladding diameter

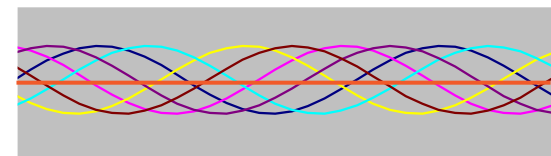
$\Lambda$ : center distance between side-core to side core

$\Lambda_{in}$ : distance between side-core center to fiber center

- This equation assumes the fiber geometry is as designed, cladding alignment is perfect ( $d = \Lambda_{in}$ ), MFD matches for MCF and SMF ( $\omega = 5 \mu\text{m}$ ), and  $\Lambda_{in} = 60 \mu\text{m}$  by design
- Thus, 1 deg angle offset will cause 0.19 dB loss, 2 deg  $\sim$  0.76 dB loss



Splicing spun multicore fiber

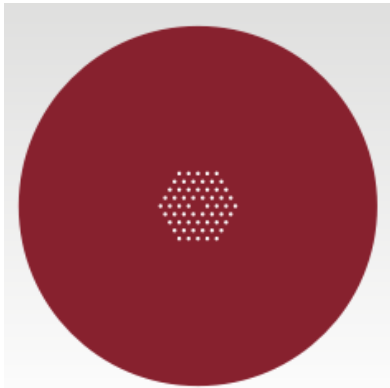


Spun multicore fiber

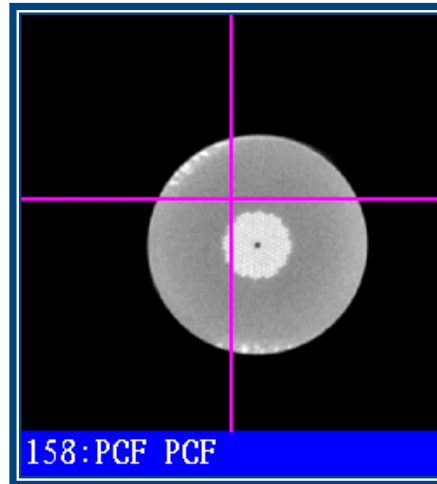
- SMF28 melts ~ 1800° C
  - Ordinary splicing
- Z-fiber melts ~ 1600° C
  - Splicing with lower power
- Chalcogenide fiber melts ~ 200 - 700° C
  - Very hard to splice with ordinary fusion splicers
  - Vaporized if no big offset
- Zblan fiber melts ~ 250° C
  - Impossible to splice with ordinary fusion splicers
  - Vaporized immediately
  - Very hard to cleave and handling



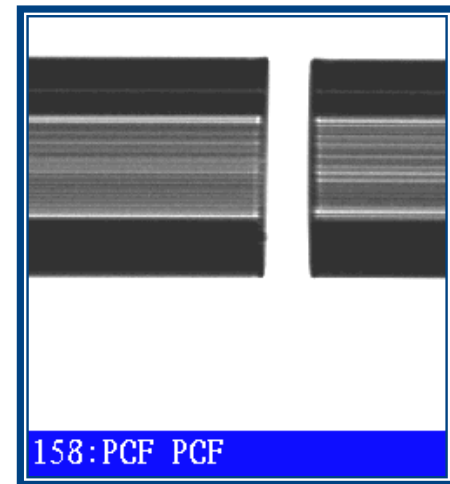
125  $\mu$ m Zblan fiber splicing



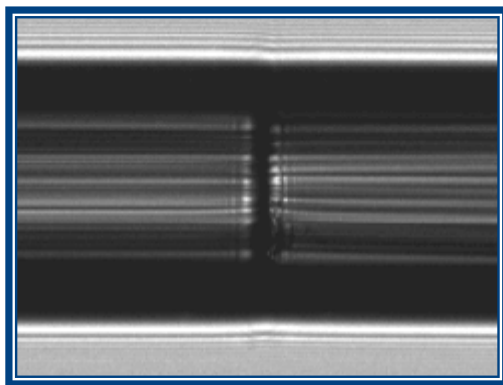
PCF with extremely small effective areas and high nonlinear coefficients for super continuum



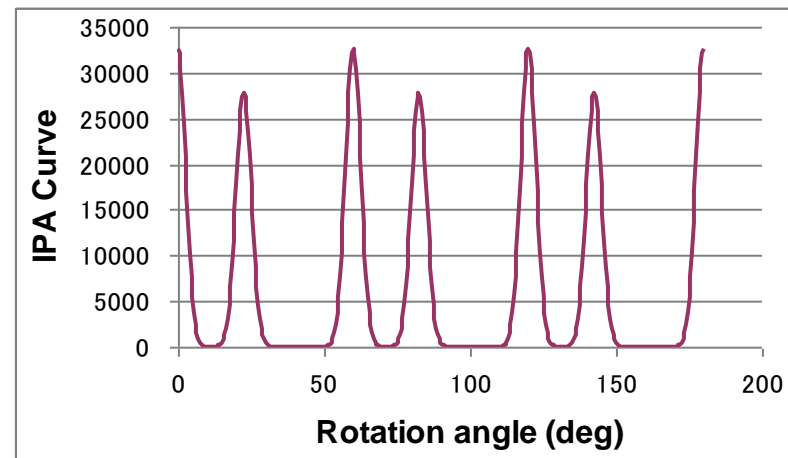
Manual alignment with end-view



Auto alignment with side-view IPA method

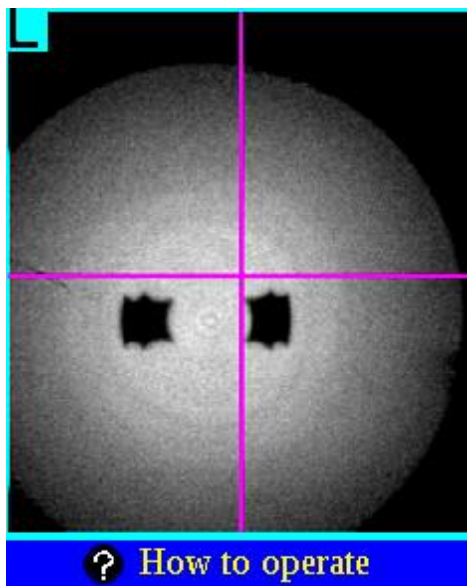


After splicing (no hole collapse) with LZM-100

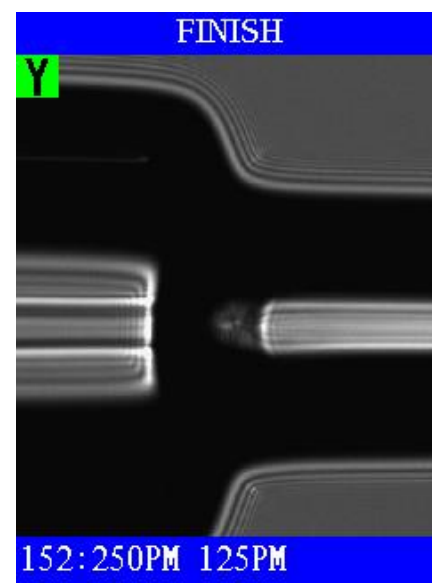
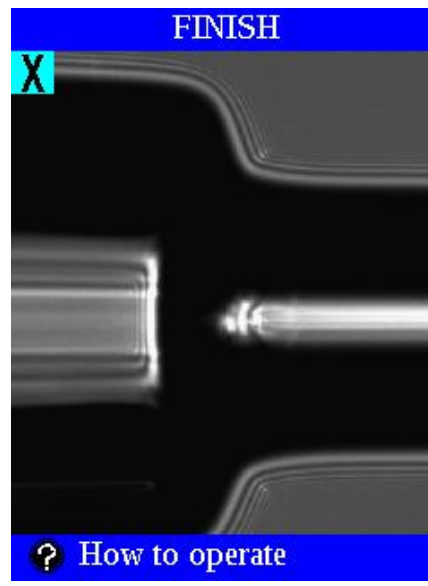


IPA curve for rotation alignment

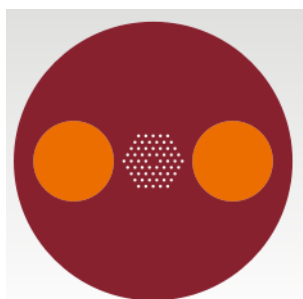
## Photonic crystal fiber aligning and splicing with end-view



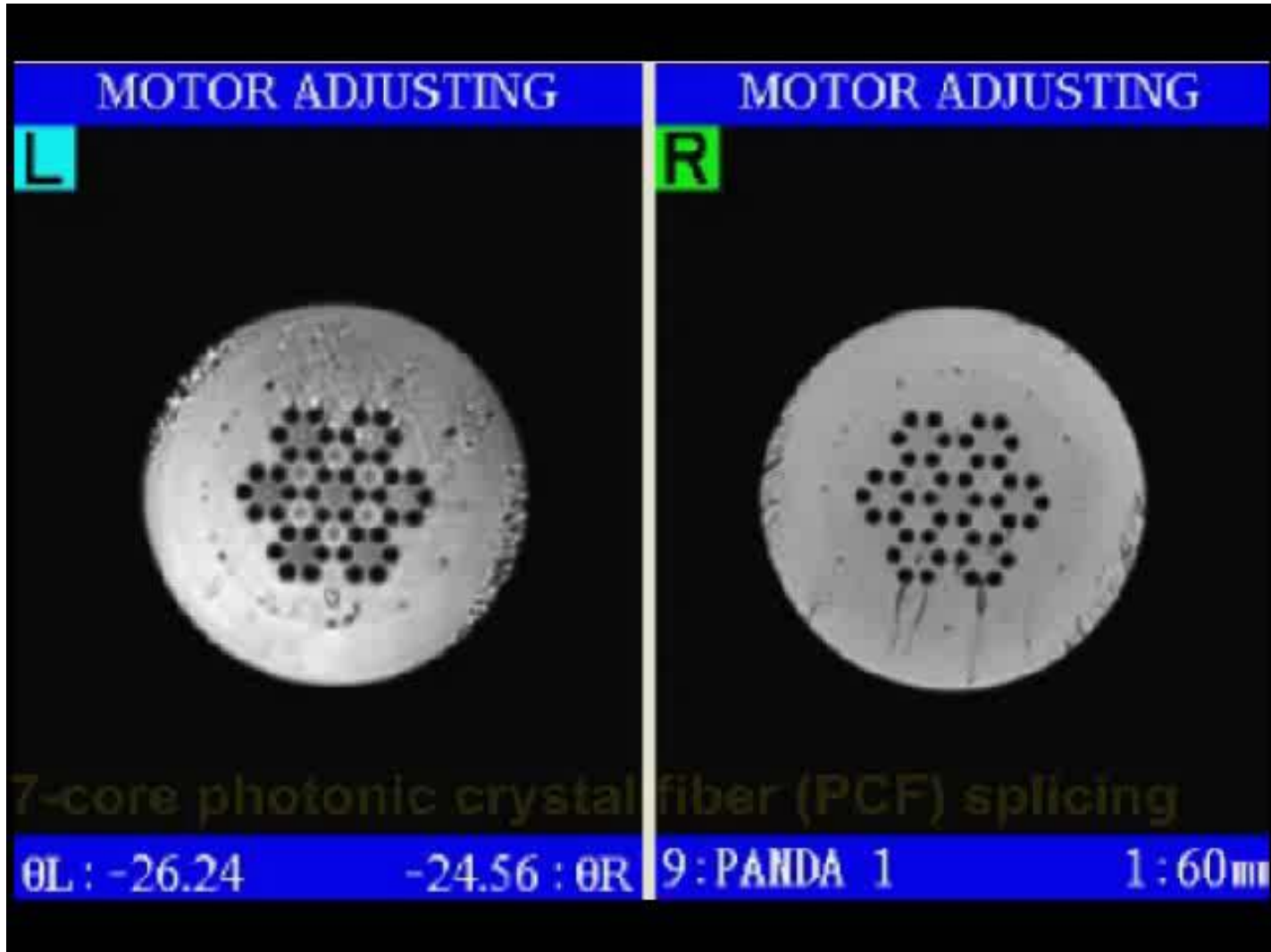
End-view alignment



After splicing



- 250  $\mu\text{m}$  large core high power PM photonic crystal fibers spliced to 125  $\mu\text{m}$  Panda fiber
- End-view manual PM alignment or side-view IPA automated PM alignment.
- Feedback core alignment with LZM-100 GPIB port







**We connect.<sup>TM</sup>**

